A Symbolic Approach to the Projection Method

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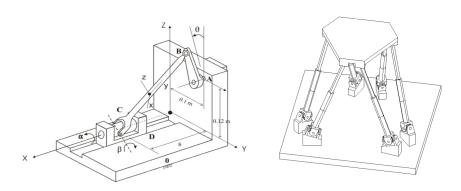
Outline

- Introduction
 - Constrained mechanical system
 - The projection method
 - Problem definition
- Our symbolic-numeric code-generating algorithm
- Experimental results

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How to do a simulation of a physical mechanical system?

- Create a model of the system
- Generate equations to describe the dynamic of the model
- Solve the equations to determine the system response



Slider Crank Mechanism and Parallel Robot

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Dynamics and kinematics of constrained mechanical system

Kinematic constraint equations

$$C(x,t)=0, (1)$$

with m nonlinear algebraic equations of n generalized coordinates $x_1, \dots, x_n \ (m < n)$.

System dynamics

$$M\ddot{x} + C_J^T \lambda = F, (2$$

4 / 21

where

- $C_{i,l}$ is the $m \times n$ Jacobian of the constraint matrix C
- M is an $n \times n$ symmetric generalized mass matrix
- λ is the $(m \times 1)$ Lagrange multiplier
- Solving these DAEs for x(t) and $\lambda(t)$ is computationally expensive

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4/21

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Symbolic computation: Allow parameters $z_1, \ldots, z_\ell \in \mathbb{R}$

- M is an $n \times n$ symmetric generalized mass matrix
- λ is the $(m \times 1)$ Lagrange multiplier
- Solving these DAEs for x(t) and $\lambda(t)$ is computationally expensive Solving these systems with parameters is extremely expensive!

The Projection Method

Blajer's (1992) projection method: hide algebraic equations from the dynamic equations:

• Find a null space basis D, an $n \times r$ matrix, such that

$$C_J D = 0 \text{ or } D^T C_J^T = 0, \tag{3}$$

• Multiply both sides of $M\ddot{x} + C_J^T \lambda = F$ by D^T

$$D^T M \ddot{x} = D^T F, \tag{4}$$

 Now we have ODEs in x and u, which can be easily solved to determine the coordinates x, velocity u, and constraint reaction λ during simulation

$$\dot{x} = Du,$$
 (5)

5/21

$$D^{T}MD\dot{u} = D^{T}(F - M\dot{D}u), \tag{6}$$

$$\lambda = (CM^{-1}C^{T})^{-1}C(M^{-1}F - \dot{D}u)$$
 (7)

Numeric vs. Symbolic Modelling and Simulation

Numeric

- Numerical matrices are used to describe the system at a given instant in time.
- Values must be given for all parameters, even if they aren't really known.
- The model must be rebuilt at every time step during simulation.

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Symbolic

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- Engineers can view the governing equations in a meaningful form
- Arbitrary substitutions for unknown quantities are not needed.

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6/21

Computer Algebra in Industrial Simulation

- MapleSim symbolic physical modelling and simulation tool
- Talk tomorrow: Symbolic Computation Techniques for Advanced Mathematical Modelling by Junlin Xu

Formal definition

Input: $A \in \mathbb{R}(z_1, z_2, \dots, z_\ell)^{m \times n}$, with $m \le n$ and rank r,

Output: straight-line code which takes parameters $\alpha_1, \ldots, \alpha_\ell \in \mathbb{R}$ and evaluates a specific (consistent) basis of the null space of A:

$$\mathbf{w}_1(\alpha_1,\ldots,\alpha_\ell), \mathbf{w}_2(\alpha_1,\ldots,\alpha_\ell),\ldots,\mathbf{w}_{n-r}(\alpha_1,\ldots,\alpha_\ell) \in \mathbb{R}^n$$

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Difficulties

- A is condensed with complex multivariate function
- Symbolic manipulation can lead to massive expression swell

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Previous proposed solutions

- Apply linear graph theory to reduce the number of equations (McPhee 2004)
- Fraction-free factoring to control the generation of large expression (Zhou, 2004)

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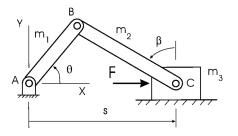
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Advantages of our approach

- Very fast
- Partial and incremental symbolic evaluation

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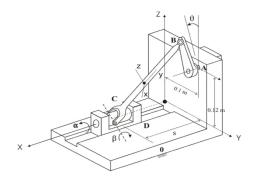
Example: Planar (2D) Slider Crank Mechanism

Planar Slider Crank Mechanism with 1 degree of freedom

$$C = egin{pmatrix} L_1 cos heta + L_2 sin eta - s \ L_1 sin heta - L_2 cos eta - s \ heta - f(t) \end{pmatrix} = 0$$

$$C_J = rac{\delta(C)}{\delta(heta,eta)} = egin{bmatrix} -L_1 sin heta & L_2 cos eta & -1 \ L_1 cos heta & L_2 sin eta & 0 \ 1 & 0 & 0 \end{bmatrix}$$

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Example: Spatial (3D) Slider Crank Mechanism

In a slightly more complicated Spatial (3D) Slider Crank Mechanism, the second column is:

$$C_{J}[*,2] = \begin{bmatrix} -L_{2} \cos(\beta) \\ -L_{2} \sin(\beta) \cos(\alpha) \cos(\theta) - L_{2} \sin(\beta) \sin(\alpha) \sin(\theta) \\ L_{2} \sin(\beta) \cos(\alpha) \sin(\theta) - L_{2} \sin(\beta) \sin(\alpha) \cos(\theta) \end{bmatrix}$$

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Example: Spatial (3D) Slider Crank Mechanism

Substitute $\sin(\alpha) = \frac{2x}{1+x^2}$, $\cos(\alpha) = \frac{1-x^2}{1+x^2}$ where $x = \tan(\frac{\alpha}{2})$:

$$J[*;2] = \begin{bmatrix} -L_2 \cdot \frac{1-X_3^2}{1+X_3^2} \\ -2L_2 \cdot \frac{(1-X_2^2)x_3(1-x_1^2)}{(1+x_2^2)(1+x_3^2)(1+x_1^2)} - 8L_2 \cdot \frac{x_2x_1x_3}{(1+x_2^2)(1+x_3^2)(1+x_1^2)} \\ 4L_2 \cdot \frac{x_2x_3(1-x_1^2)}{(1+x_2^2)(1+x_3^2)(1+x_1^2)} - 4L_2 \cdot \frac{(1-x_2^2)x_3x_1}{(1+x_2^2)(1+x_3^2)(1+x_1^2)} \end{bmatrix}$$

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Our algorithm

Sketch of our approach

Computing the null space using LU decomposition in a hybrid symbolic-numeric fashion

- Choose the ordering of row and column interchanges using "indicative" numerical values
- Perform a symbolic LU decomposition of the "permuted" A without pivoting
- Generate straight-line code to evaluate a null space basis at any setting of the parameters

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Algebraic static pivot selection

Strategy for pivot selection

- **1** Choose "random" values $\alpha_1, \ldots, \alpha_\ell$ of parameters z_1, \ldots, z_ℓ from a finite subset $S \subseteq \mathbb{C}$:
- 2 Return P, Q such that $P \cdot A(\alpha_1, \ldots, \alpha_\ell) \cdot Q$ has an LU-decomposition (without pivoting), using Gaussian Elimination with complete row/column pivoting.
 - I.e., just record the row/column pivot selection.
 - Good news: the probability of success is high (Schwarz-Zippel Lemma)
 - Bad news: Choosing random points might be be numerically unstable...

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Numerical static pivot selection

Remember: Gaussian elimination is relatively stable with complete pivoting, where we always choose the largest pivot

Strategy: Choose the "largest" pivot via random evaluations

We offer two heuristic approaches given for choosing pivot:

- Evaluation at real values to assess the degree of the pivot function
- Evaluations at random points off the unit circle to get an idea of coefficient size

Overall heuristic:

- Choose 4 random evaluations (2 real, 2 on unit circle)
- Perform 4 simultaneous Gaussian Eliminations, same pivoting choices
 - Choose a pivot which makes all evaluations large (or start over)

13 / 21

Choosing pivots in the spatial slider crank example

We perform Gaussian elimination with complete row-column pivoting simultaneously on 4 random evaluations of $A(z_1, z_2, z_3)$:

$$A(\omega_1^2,\omega_2^2,\omega_3^2) = \begin{bmatrix} 0.0 & 7.7405\text{e-}12 - 1.4447\text{e-}1i & 0.0 & 1.07 \\ -5.1923\text{e-}1 + 3.7140\text{e-}10i & 1.2421\text{-}8.6191\text{e}-10i & 3.9562\text{e-}1 - 8.7185\text{e-}2 & 0.0 \\ 3.5456\text{e-}10 + 5.3896\text{e-}1i & -8.5540\text{e-}10 - 1.19671i & -1.4832\text{e-}1 - 4.6630\text{e-}1i & 0.0 \\ A(\omega_1^1,\omega_2^3,\omega_3^6) = \begin{bmatrix} 0.0 & 4.8246\text{e-}11 - 1.3143i & 0.0 & 1.07 \\ 4.7239\text{+}1.7945\text{e-}9i & 5.0294\text{+}2.4527\text{e-}9,i & -4.8475 + 8.7185\text{e-}2i & 0.0 \\ -1.7148\text{e-}9 + 4.9033i & -2.9437 + 4.8454i & -1.4832\text{e-}1 - 4.9760i & 0.0 \end{bmatrix}$$

$$A(2.0,3.0,4.0) = \begin{bmatrix} 0.0 & 0.2647058824 & 0.0 & 1.0 \\ -0.07411764706 & -0.1355294118 & 0.2301176471 & 0 \\ -0.2541176470 & 0.03952941175 & 0.2461176470 & 0.0 \end{bmatrix}$$

$$A(4.0,3.0,5.0) = \begin{bmatrix} 0.0 & 0.2769230769 & 0.0 & 1.0 \\ 0.0423529411 & -0.1140271494 & 0.1136470589 & 0 \\ -0.2736651585 & -0.01764705884 & 0.26656651585 & 0 \end{bmatrix}$$

Get the following two permutation matrices from the pivots

$$P = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix}, \quad Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \end{bmatrix}$$

So *PAQ* has a strict LU decomposition, and it is numerically robust (at least at these 4 points...but heuristically most of the time)

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Step 2: Generate straight-line code for the null-space

We have quickly determined permutation matrices P, Q such that

$$PAQ = LU$$
 where $U \in \mathbb{R}(z_1, \dots, z_\ell)^{m \times m}$ lower triangular, $U \in \mathbb{R}(z_1, \dots, z_\ell)^{m \times n}$ upper triangular

- A specific null-space basis determined by last n r columns of the computed U
- Evaluated U at $\alpha_1, \ldots, \alpha_\ell$ to instantiate null-space basis
- Completely straight-line code no decisions to make
- Procedure works with high probability: essentially when $U_{ii}(\alpha_1, \dots, \alpha_\ell) \neq 0$, which is "almost all the time"
 - use Schwarz-Zippel Lemma to be more precise

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Heuristic numerical performance

We have quickly determined permutation matrices P, Q such that

$$PAQ = LU$$
 where $U \in \mathbb{R}(z_1, \dots, z_\ell)^{m \times m}$ lower triangular, $L_{ii} = 1$ $U \in \mathbb{R}(z_1, \dots, z_\ell)^{m \times n}$ upper triangular

- Numerically good when $U_{ii}(\alpha_1,\ldots,\alpha_\ell)$ "large enough"; these are the pivots
- When choosing the pivots, want the rational functions U_{ii} to be "large enough"
- Idea: the size of random values reflects the size of the rational function (coefficients and degree) with high probability
- Support:
 - Numerical Schwartz-Zippel similar to Kaltofen, Yang, Zhi (2007)

16 / 21

- Real evaluation in floating point estimate degree
- Gaussian elimination with static pivoting: Li & Demmel (1998)

Time efficiency with typical multibody models

Models	C_J imensions	No. of parameters
Planar Slider Crank	4 × 3	3
Planar Seven Body Mechanism	7 × 6	7
Quadski Turning	19 × 11	16
Hydraulic Stewart Platform	24 × 18	41

Multibody models from MapleSim

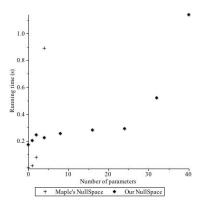
Models	Maple	Hybrid
Planar Slider Crank	0.046s	0.016s
Planar Seven Body Mechanism	0.078s	0.031s
Quadski Turning	timeout (>200s)	0.56s
Hydraulic Stewart Platform	timeout (>200s)	1.64s

Running time (in seconds)

Remember: we are only evaluating at one point (with C code)

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Running time with different numbers of parameters



Running time on Hydraulic Stewart Platform with different numbers of parameters

Important advantage: we can easily instantiate more or fewer parameters, and evaluate the same nullspace.

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Models	C_J dimensions	Size of straight-line code
Planar Slider Crank	3 × 4	5671
Planar Seven Body	6 × 7	75045
Quadski Turning	11 × 19	41706824
Hydraulic Stewart Platform	18 × 24	11849101

The final straight-line code can be greatly simplified by

- Common expression identification
- Trigonometric simplification

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Example of the straight-line code for Slider-Crank Mechanism

Straight-line code for Spatial Slider-Crank Mechanism

Optimized straight-line code using Maple's CodeGeneration

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Summary

- We have proposed a hybrid symbolic-numeric algorithm to compute the null space basis of a multivariate matrix.
- Our approach is significantly faster than computing null space symbolically, making it applicable to use in symbolic modelling and simulation.
- By using static pivot selection, our straight-line code for generating the null space is numerically robust at almost all parameters settings.

Future Challenges

- More robust numerical methods
 - Iterative refinement (from Li & Demmel 1998)
 - Wiser pivot selection
- Better code generation

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The ultimate goal of this research

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